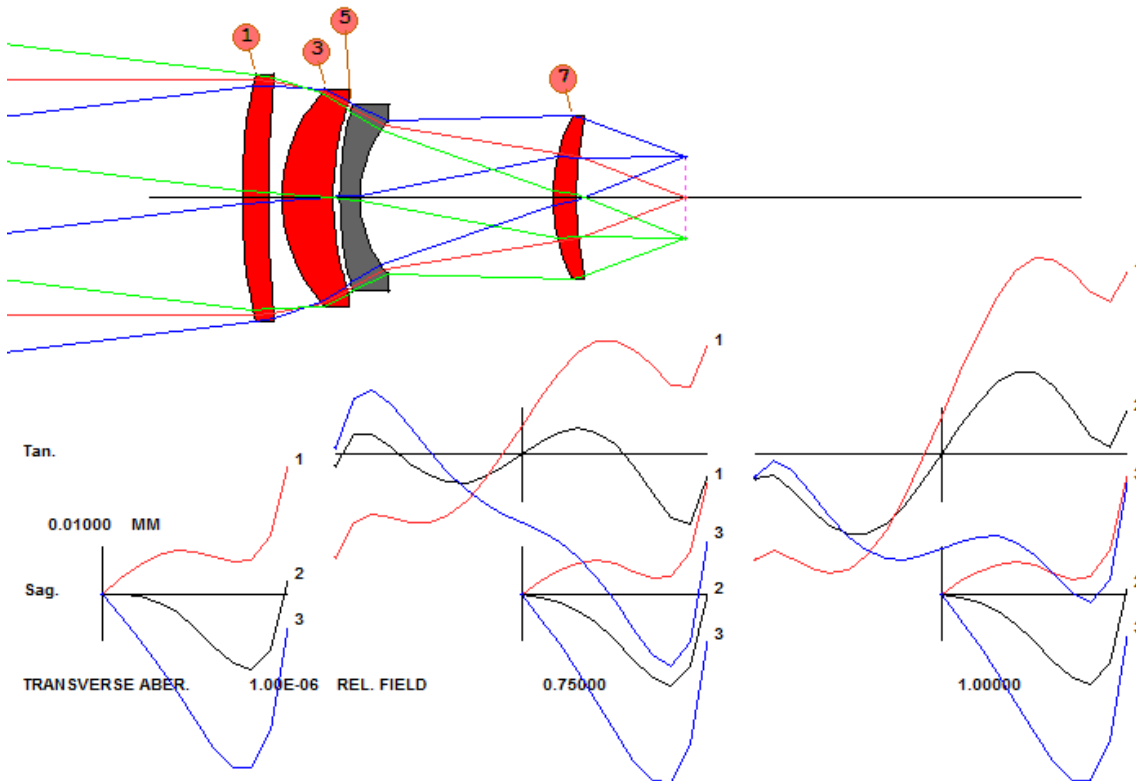


Lesson 10: Near-IR Lens Example

Lesson 8 showed how to design an apochromatic objective for use in the visible spectrum. Now we will design one for the near infrared over the wavelength range from 1.06 to 1.97 μm .

The challenge when designing a lens for the infrared is finding optical materials that are useful over the spectral range and whose cost and chemical properties are attractive. The task in this lesson is to redesign an existing lens, replacing some undesirable materials with ordinary optical glass. The reference system is bundled as 1.RLE, with the ID MIT 1 TO 2 UM LENS. You can **FETCH** that lens and examine its performance. Set the scale of the Fans curves to 0.01 mm.



That lens has three elements of ZNS and one of AS2S3, making four elements in all. Those names refer to zinc sulphide and arsenic trisulphide glass, and we would like to avoid those materials if possible. The first-order properties we need to match are as follows (dimensions are in mm):

- Entering beam radius 17.5
- Chief-ray angle 0.935 degrees
- Back focus distance 16.3
- Cell length 50

The Plan of Action

Rather than try to change the materials in the present lens, all of which have an index greater than 2.0, let us start from scratch. For this we will use the design search program. But first we have to be somewhat choosy: if we just run **DSEARCH** and let it find model glasses, it will not come back with any of the unusual glasses that make a big difference in the NIR. (The model represents an *average* of all glasses.) So we have to steer it. Open the glass table display (**MGT**), select the Guangming table, and then click the Graph button and select the option shown.


```

CORE 16
PROJ
DSEARCH 3 QUIET      ! the best lens will show up in library location 3 (and also in PAD)
SYSTEM              ! system requirements follow
ID NIR EXAMPLE      ! lens identification
OBB 0 .935 17.5     ! specify the object
WAVL 1.97 1.53 1.06 ! and the wavelength range
UNITS MM
END

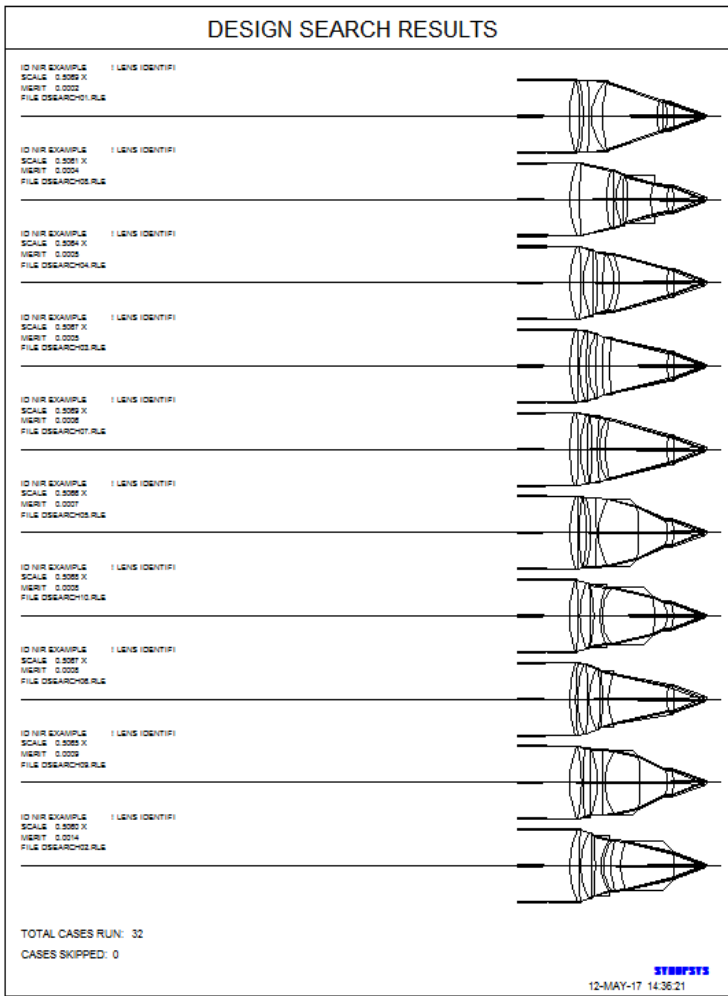
GOALS                ! here we set the goals
ELEMENTS 5           ! since glass has a lower index, we'll ask for 5.
FNUM 1.428
BACK 16 .1
TOTL 50 .1
STOP FIRST          ! there seems to be no reason to let the stop position vary
STOP FIX            ! so we put it in front and keep it there
NPASS 100
ANNEAL 200 20
RSTART 300          ! a useful starting radius,
TSTART 1            ! and this thickness on each element to start with
QUICK 60 90
FOV 0 .5 1
FWT 2 1 1
GLASS POS           ! positive elements will use this glass type
G D-FK61
GLASS NEG           ! and negative this type.
G H-ZF88
END

SPECIAL            ! here we give requirements that are not defaults
ACM 3 .1 1         ! auto edge control (AEC) and center thickness control (ACC) are defaults
ACA                ! but we add to these ACM, so thicknesses do not get too thin, ACA,
ASC                ! so rays do not approach the critical angle, and ASC so surfaces do not
END                ! get too close to the hemisphere point.

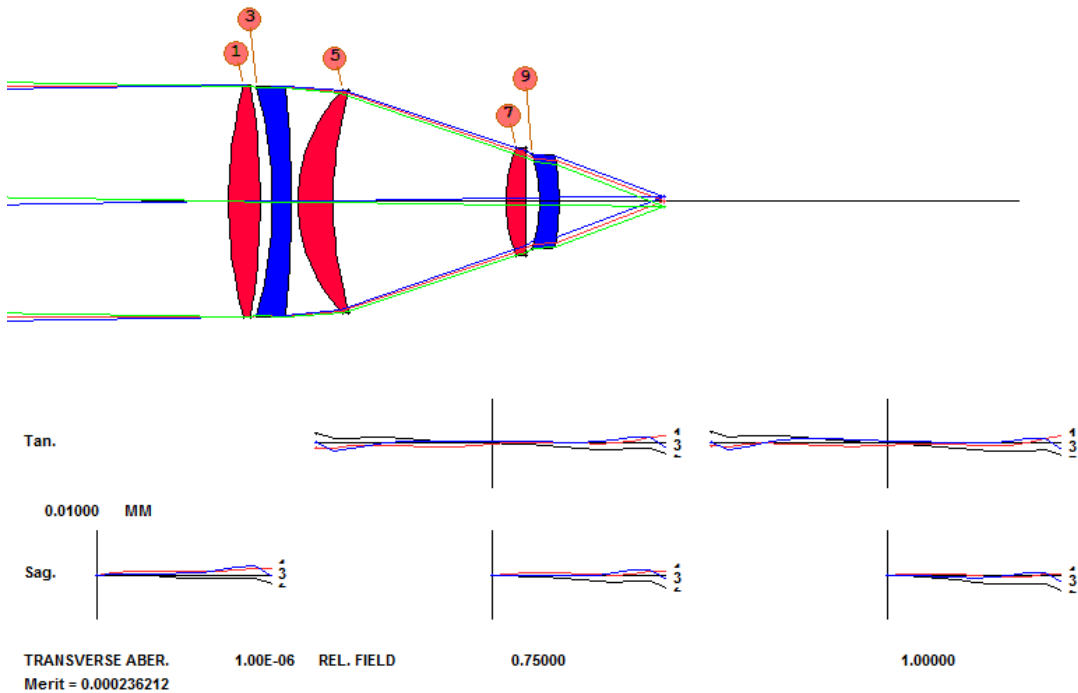
GO                 ! this starts the process.
PROJ

```

In less than a minute, the process produces a picture of the 10 best configurations it found.



We now have a very good 5-element lens, but it has only the two glass types we specified. It's time to do a more comprehensive search.



Look at the MACro DSEARCH_OPT .MAC, which DSEARCH has conveniently constructed for us and should be open in a new editor window.

```
PANT
VLIST RD ALL
VLIST TH ALL
END
AANT P
AEC
ACC
GSR      0.000000      2.000000      4 M      0.000000
GNR      0.000000      1.000000      4 M      0.500000
GNR      0.000000      1.000000      4 M      1.000000
M  0.160000E+02  0.100000E+00 A BACK
M  0.500000E+02  0.100000E+00 A TOTL
  ACM 3 .1 1 ! AUTO EDGE CONTROL (AEC) AND CENTER THICKNESS CONTROL (ACC) ARE DEFAULTS
  ACA          ! BUT WE ADD TO THESE ACM, SO THICKNESSES DO NOT GET TOO THIN, ACA,
  ASC          ! SO RAYS DO NOT APPROACH THE CRITICAL ANGLE, AND ASC SO SURFACES DO NOT
END
SNAP/DAMP 1
SYNOPTSYS 100
```

Save this MACro with the name NIR_OPT.MAC. This is the optimization MACro that will be run over and over when we execute **GSEARCH**, which will determine which glass should go on which elements. Now make a new MACro (type **AEE** to open a new editor, and type the data below)

```
CORE 16

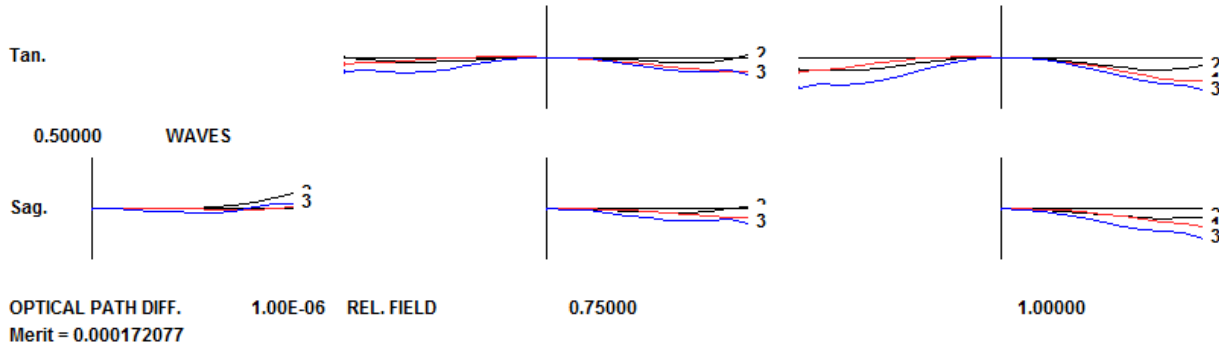
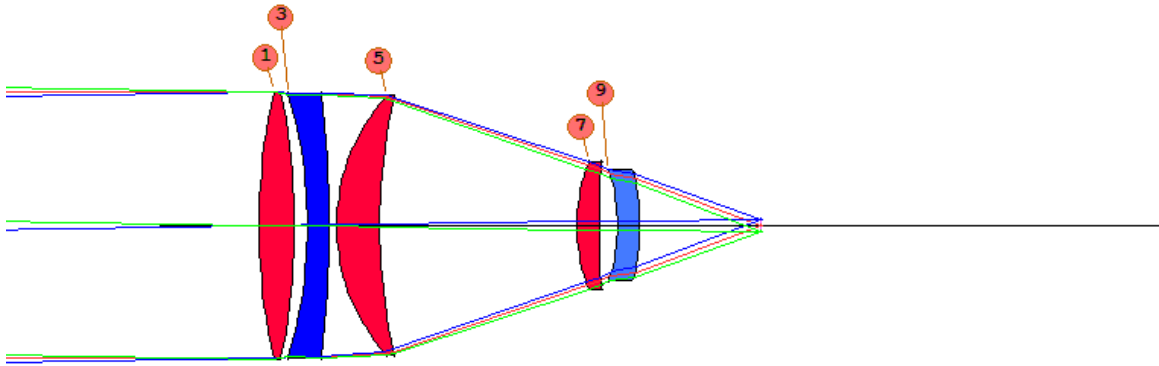
GSEARCH 3 QUIET LOG

SURF
1 3 5 7 9
END

OFFILE 'NIR_OPT.MAC'
NAMES
G G-ZF52
G D-FK61
G H-ZF88
G H-F51

END
USE 2
GO
```

The lens has improved even more. The performance is now just over 0.2 waves of aberration everywhere.



It looks like we have a solution! There is almost no primary or secondary chromatic aberration. We have succeeded in replacing the undesirable materials with ordinary glass, and the performance became much better than the original at the same time.

Mission accomplished! Here is a SPEC listing of the final lens:

SYNOPTSYS>SPE

ID NIR EXAMPLE
 ID1 DSEARCH CASE WAS 000000000000000000010110 22
 LENS SPECIFICATIONS:

SYSTEM SPECIFICATIONS

OBJECT DISTANCE (TH0)	INFINITE	FOCAL LENGTH (FOCL)	49.9800
OBJECT HEIGHT (YPP0)	INFINITE	PARAXIAL FOCAL POINT	15.9992
MARG RAY HEIGHT (YMP1)	17.5000	IMAGE DISTANCE (BACK)	15.9992
MARG RAY ANGLE (UMP0)	0.0000	CELL LENGTH (TOTL)	50.0025
CHIEF RAY HEIGHT (YPP1)	0.0000	F/NUMBER (FNUM)	1.4280
CHIEF RAY ANGLE (UPP0)	0.9350	GAUSSIAN IMAGE HT (GIHT)	0.8157
ENTR PUPIL SEMI-APERTURE	17.5000	EXIT PUPIL SEMI-APERTURE	24.7688
ENTR PUPIL LOCATION	0.0000	EXIT PUPIL LOCATION	-54.7406

WAVL (uM) 1.970000 1.530000 1.060000
 WEIGHTS 1.000000 1.000000 1.000000
 COLOR ORDER 2 1 3
 UNITS MM
 APERTURE STOP SURFACE (APS) 1 SEMI-APERTURE 17.53054
 FOCAL MODE ON
 MAGNIFICATION -4.99800E-11
 POLARIZATION AND COATINGS ARE IGNORED.
 SURFACE DATA

SURF	RADIUS	THICKNESS	MEDIUM	INDEX	V-NUMBER
------	--------	-----------	--------	-------	----------

0	INFINITE	INFINITE	AIR			
1	83.04964	4.55863	D-FK61	1.48647	78.02	GUANGMIN
2	-90.13577	1.76097	AIR			
3	-61.20988	2.89016	H-ZF88	1.87811	26.89	GUANGMIN
4	-136.80545	1.00000	AIR			
5	26.01458	5.71573	D-FK61	1.48647	78.02	GUANGMIN
6	83.59388	25.92496	AIR			
7	24.21580	2.91205	D-FK61	1.48647	78.02	GUANGMIN
8	117.43058	2.36412	AIR			
9	-24.23661	2.87587	H-F51	1.60755	25.46	GUANGMIN
10	-40.27187S	15.99923S	AIR			
IMG	INFINITE					

KEY TO SYMBOLS

A	SURFACE HAS TILTS AND DECENTERS	B	TAG ON SURFACE
G	SURFACE IS IN GLOBAL COORDINATES	L	SURFACE IS IN LOCAL COORDINATES
O	SPECIAL SURFACE TYPE	P	ITEM IS SUBJECT TO PICKUP
S	ITEM IS SUBJECT TO SOLVE	M	SURFACE HAS MELT INDEX DATA
T	ITEM IS TARGET OF A PICKUP		

THIS LENS HAS NO SPECIAL SURFACE TYPES
THIS LENS HAS NO TILTS OR DECENTERS
SYNOPSIS>

If these lenses are okay mechanically, the problem is solved.

Except ... what is the transmission at 1.97 microns? Type **FIND TRANS IN COLOR 1**. It comes back 98.18%. (Coatings are ignored here because the lens is not in polarization mode.) Very good!

But what if the value had come back too low? Well, then go back to the glass map and display the absorption at 1.97 microns – and select glasses with shorter data bars. Lens design is all about tradeoffs, after all, and with these tools one can get the best one rather easily.